



Comparative Studies of Adsorption of Heavy Metals from Cement Waste Water Using Activated Carbon from Palm Kernel Husk, Coconut and Groundnut Shells

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ABSTRACT: Cement waste water is a major source of heavy metal pollution which requires removal before disposal. This paper therefore evaluates the comparative adsorption of heavy metals from cement waste water using activated carbon from palm kernel husk, coconut and groundnut shells in line with standard methods. With 0.1M KOH as activating agent at 400 °C, PKH and GNS reduced zinc concentration in water from 0.06mg/l to 0.01mg/l while CCS reduced iron concentration by 50% for temperature range of 450 °C – 500 °C. However, when 0.1M ZnCl was used as activating agent, all three adsorbents reduced the concentration of Zn, Fe and Pb to 0.01mg/l within the temperature range of 400 °C – 450 °C while Nickel was substantially reduced to 0.01mg/l by all three adsorbents with 0.2M ZnCl as activating agent for temperature range of 400 °C to 500 °C. The result shows that all three materials could serve as adsorbents but their performance depends on temperature and activating agents. For palm kernel husk and coconut shell, their performance was inversely proportional to temperature, while groundnut shell shows a direct relationship. On the overall, the three precursors showed capacity as good adsorbent for treatment of cement waste- water.

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The place of cement in the satisfaction of man's quest for structural and other forms of modern development is enormous (European cement association, 1996). However, cement production comes with serious environmental challenges like those arising from the waste water which is laden with heavy metals and other complex mixtures of chemicals which can trigger consequential changes in critical water qualities (Francis *et al.*, 2014). In the consideration of water contaminants, heavy metals take the front row because they are especially dangerous, highly persistence and toxic (Gonzalo *et al.*, 2010). They are hazardous to the biotic environment with adverse impact on vegetation, human, animal health and the eco system (Pandey *et al.*, 2014; Radia *et al.*, 2018). Also, excessive concentrations of heavy metals in the environment may harm human health, and its usage may leave dust deposits in eyes, ears and nasal passages, and may cause injury to the skin or mucous membranes. They also lower reproductive success, prevent proper growth and development and even cause death (Nur *et al.*, 2014). They are non-biodegradable and could distort enzyme function by attracting and forming bond with sulphur. However, due to the associated high cost of conventional treatment operations, cement producing companies

now adapt some alternative measures in the management of their waste water. For example, in 2007, Dangote cement plant Gboko, had to re-inject more than 80% of its waste water into petroleum reservoirs (Wan *et al.*, 2008) while about 18% was disposed into the environment. However, recycling of untreated waste water have the capacity to cause further problems like clogging of reservoir pores and making it difficult to continue to use such reservoir as water dumps. In a bid to avert the seeming high cost in conventional water treatment that may negatively affect cost of product and thus affect the Company's chances of remaining in business, the Oinyi River (situated in the Confluence town in Kogi and linked to river Niger and River Benue) which hitherto had served the people of North Central Nigeria for both domestic and industrial purposes is now being constantly perturbed by waste water from a cement industry. The degree of impact of this waste- water on the water quality is presently unknown as there is no documented information (Francis *et al.*, 2014). However, there are reports of several disease outbreaks, unusual deaths and poor agricultural output around the area in recent times and other serious environmental damage as a result of improper treatment of waste water released to the environment

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from the cement industries in the state (Nwankwo et al., 2014). Conventional cement waste-water treatment has involved the application of unit operations or unit processes such as chemical precipitation, coagulation, adsorption, ion exchange and membrane filtration (Gregg and Singh, 2002; Mohan and Singh, 2002) Furthermore, among the aforementioned treatment technologies, adsorption has been reported as an efficient and economic option because of convenience and ease of operations and simplicity of design (Chengwen et al., 2014).

Although a number of adsorbent materials have been studied for their adsorptive abilities with some relatively promising success for the elimination of heavy metals from wastewater using various agricultural waste such as sugarcane bagasse, rice husk, oil palm shell, coconut shell, coconut husk etc (Lim and Aris, 2014 ; Nasim *et al.*, 2004). The objective of this research is to study and compare the adsorptive capacities of activated carbon from coconut shell, groundnut shell and palm kernel husk for the removal of Zn, Fe, Pb, Cr and Ni from cement waste water.

MATERIALS AND METHODS

The adsorbates solution of Zn, Fe, Pb, Cr and Ni metal ions were prepared from analytical grade $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$, $\text{Pb}(\text{NO}_3)_2$, $\text{Cr}(\text{NO}_3)_3$ and $\text{NiCl}_2 \cdot 6\text{H}_2\text{O}$ following the method of Agbozu and Emoruwa, (2014). The precursors, coconut shells, palm kernel husks and groundnut shells (CCS, PKH and GNS respectively) obtained from Effurun market, in Delta State were washed using tap water to remove dirt and sands. The washed sample materials were sun dried for five (5) days and then pelletized into fine particles with the aid of a manual grinder and sieved to 120 mm mesh size - a physical treatment method. Similar method was reported by Agbozu and Emoruwa, (2014) in their experiment on batch adsorption of heavy metals (Cu, Pb, Fe, Cr, and Cd) from aqueous solutions using coconut husk.

The furnace (DAIHAN-brand® programmable Tube Furnace) was set at a temperature of 500 °C. Then each of the sample materials placed in a crucible, was transferred to the muffle furnace (DAIHAN-brand® 1,200 °C Digital Muffle Furnace) for 2 hours to be carbonized. Carbonization increases the percentage of carbon in the adsorbents due to the loss of moisture content and volatile compounds. This is in line with Nur et al., (2014).

After two (2) hours of heating, the carbonized samples were each divided into four (4) parts in crucibles labeled A to D and allowed to cool. Samples in crucibles A to D were subsequently

activated(chemical treatment) in the ratio of 2:3 (mass of sample: mass of activating agent) using 0.1 M KOH, 0.2 M KOH, 0.1 M ZnCl_2 , and 0.2 M ZnCl_2 respectively at 400 °C, 450 °C and 500 °C for three hours. All chemicals used were of analytical grades. The samples were then brought out of the muffle furnace and cooled in desiccators, after which they were washed several times with distilled water using a funnel and filter paper until a pH (measured using a Scout pro, ohaus, London pH meter) range between 5 and 6 was obtained. The adsorbent was then dried in an oven (Carbolite Gero High Temperature Laboratory Oven - LHT) at 170 °C for a period of 2 hours. Similar procedure was used by Bernard et al., (2013) in their studies on heavy metals removal from industrial wastewater by activated carbon prepared from coconut shells.

Batch adsorption of zinc, iron, chromium, lead and nickel from cement waste water was carried out to determine the adsorption capacity of activated carbon produced from the different plant materials, activated as highlighted above under the specified temperatures. The activated carbon (10 mg, measured using Scout pro, Ohaus, London weighing balance) was added to 120 ml of the waste water, agitated and allowed to contact for 180mins since the optimum contact time for PKH, GNS and CCS was 120mins to 240mins from studies by Elijah *et al.*, 2009, William et al., 2016 and Chengwen *et al.*, (2014). The mixture was then filtered using a filter paper into a 250 ml beaker (Pyrex, England). The filtrate was analyzed to ascertain the concentration of heavy metals left using the Atomic Absorption Spectrophotometer (AAS) (Claisse LeNeo Fluxer). The control sample was untreated (UTD) cement wastewater with no adsorbent applied. After equilibrium was attained, the metal uptake capacity for each sample was calculated using values obtained from a mass balance measurement of the metal ion and applying the equation 1 in line with Eruola and Ogunyemi, (2014).

$$q_e = (C_o - C_e) \times \frac{V}{m} \quad 1$$

Where m the mass of adsorbent (g) is, V is the volume of the solution (l), C_o is the initial concentration of metal (mg/l), C_e is the equilibrium metal concentration (mg/l) and q_e is the metal quantity adsorbed at equilibrium (mg/g).

The percent removal of metal ions from the solution was calculated using equation 2.

$$\% \text{ removal} = \frac{(C_o - C_e)}{C_o} \times 100 \quad 2$$

Hence, the amount of un-adsorbed metal ion (mg/l) = 1 - % removal of metal ions from their solutions.

RESULTS AND DISCUSSION

Figures 1 to 2 show the results of the adsorbents (PKH, CCS, and GNS) activated with 0.1 M KOH for the adsorption of Zinc, Iron, Chromium, Lead and Nickel from the cement waste water as well as the control sample. Figure 1(a) specifically compared the performance of the three adsorbents produced at different activation temperatures on the removal of Zinc from the waste water. It was observed that at 400 °C, PKH and GNS performed well giving 0.01mg/l each of un-adsorbed Zinc while 0.03mg/l was recorded for CCS. However, as the activation temperature increased from 400 °C to 450 °C and then 500 °C, the performance of PKH and GNS was observed to decrease giving concentrations of un-adsorbed Zinc of 0.04 mg/l, 0.05 mg/l and 0.03 mg/l, 0.04 mg/l respectively which indicates that the adsorption process is exothermic as commonly observed for organic adsorbents. It also suggests that the process may be physically driven (physical adsorption) and thus the resultant intermolecular forces between adsorbate and adsorbent are much weaker than those between adsorbate and solvent (Vinod et al., 2017). For CCS, it showed improvement in performance for higher temperatures (as above) giving the concentrations of un-adsorbed Zinc metal of 0.02 mg/l and 0.01 mg/l. This suggests a chemisorption process since increase in temperature results in increase in chemical reaction where increased temperature chemically changes the adsorbent and its adsorption sites/surfaces, capacity and activity. Also, the favorable intermolecular forces between adsorbate and adsorbent seem much stronger than those between adsorbate and solvent. This shows that the performance of the adsorbents for the removal of Zinc metal is a function of the activation temperature. Similar result was obtained by Al-Degs et al., (2007), for adsorption capacity of activated carbon for reactive dyes.

Figure 1(b) describes the removal of Iron at the different temperatures using the three adsorbents. PKH showed a consistent performance at all temperatures implying that temperature may not really affect its performance in the removal of Iron as the process seems likely to be more of a physical adsorption where the resultant intermolecular forces between adsorbate and adsorbent maintained a much weaker status compared to those between adsorbate and solvent irrespective of temperature. CCS gave a sharp improvement in performance as the amount of un-adsorbed Iron metal reduced by 50% on increased

temperature from 400 °C to 500 °C. This suggests a case of chemisorption as increase in temperature seems to positively affect the reaction rate. A report by Abdurasaq and Basiru, (2010) showed a similar trend of $94\% \pm 1.4\%$ removal efficiency of Fe (III) ions from mono-component simulated waste effluent using coconut husk. GNS seems to be inconsistent in behavior for iron removal as temperature increased from 400 °C to 500 °C. This suggests that application of GNS in iron removal is sensitive to temperature and seems to require specific activation temperature for optimum performance.

Figure 1(c) shows the removal of Chromium using the adsorbents within the temperature range. PKH and GNS show exothermic character suggesting a physical adsorption processes while for CCS, it was observed that optimum performance is clearly selective of temperature as activation sites are likely to become more and readily available at specific temperatures (Omar, 2011; Radia et al., 2018). The exceptional performance observed at 450 °C is indicative of the process temperature preference as there was no marked difference in the performance at 400 °C and 500 °C.

Figure 2(a) highlights the removal of Lead under same conditions as above. The trend observed seems to be consistent for all three adsorbents as increasing temperature increased the performance of the adsorbents in Lead removal. As highlighted in discussing Figure 1, increasing temperature enhances reaction rate which suggests a chemical adsorption process. While all three adsorbents performance for the first time in this study maintained a consistent profile, the performance rating seems to favor GNS followed by CCS and PKH.

For the 0.1M KOH treated adsorbents, Figure 2(b) highlights the removal of Nickel. It was observed that the removal of Nickel using PKH reduced but there was an observable increase with GNS as temperature increased suggesting physical and chemical processes respectively while CCS showed a consistent performance irrespective of change in temperature. This behavior could be due to (1) the surface area modification activity of the activating agent not in being in favor of the adsorption capability of the adsorbents at higher temperatures (2) the possibility of intermolecular interaction between the adsorbate (Nickel ions) and the surface of the adsorbent not supporting nickel adsorption and (3) the possibility of the resultant pore sizes of adsorbent occasioned by increasing activation temperature and activating agent not being able to freely accommodate the size of Nickel

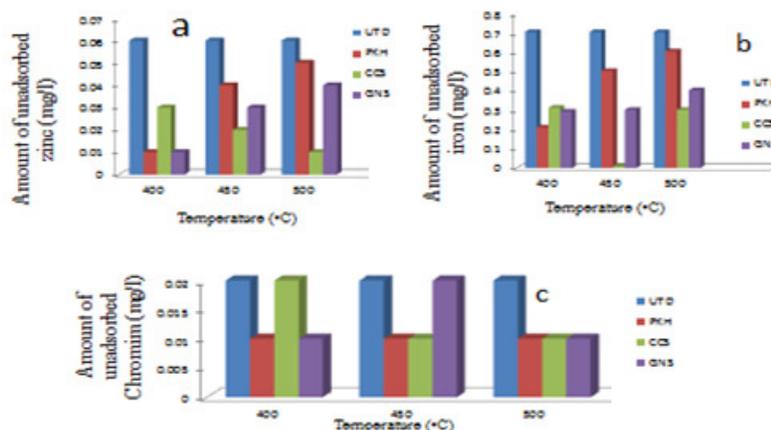


Fig 1. Amount of un-adsorbed (a) zinc (b) iron (c) chromium for 0.1 M KOH with palm kernel husk (PKH), coconut shell (CCS), groundnut shell (GNS) as adsorbent and untreated (UTD)

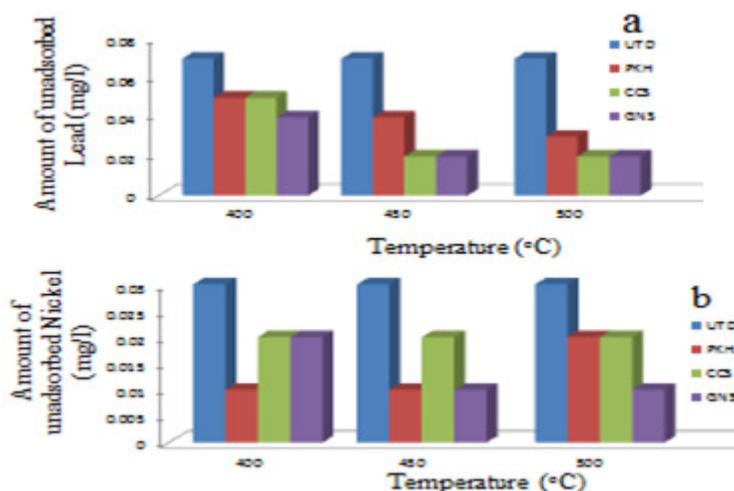


Fig 2: Amount of un-adsorbed (a) zinc (b) lead (c) nickel for 0.1 M KOH with palm kernel husk (PKH), coconut shell (CCS), groundnut shell (GNS) as adsorbent and untreated (UTD)

Figures 3 to 4 show the performance of the different adsorbents treated with 0.2 M KOH activated at temperatures of 400 °C, 450 °C and 500 °C. Figure 3(a) specifically highlights the performance of the adsorbents at the different temperatures in the removal of Zinc metal. The result shows that as temperatures increases, increasing KOH from 0.1 M to 0.2 M did not translate to increase in the adsorption of Zinc by any of the adsorbents compared to the case of 0.1 M which gave considerably lower un-adsorbed zinc concentration by the different adsorbents at different temperatures. This could be attributed to the fact that metal ions are more soluble at lower pH values and this increases their adsorption as observed by Olayinka et al., (2009). Removal of metal ions at higher pH values could be attributed to the formation of their hydroxides which results in precipitates, this is consistent with the observation of Lisa et al., (2004) and Xiao and Ju-Chang, (2009). Therefore, removal of

metal ions at higher pH values is due to precipitation rather than adsorption (Kim et al., 2005). This suggests that 0.1 M may be the optimum concentration of KOH for activation of these adsorbents for Zinc removal. This is due to the fact that the micropores are most developed in the internal void structure of activated carbon using 0.1M KOH. (Yang et al., 2017) Figure 3(b) shows the performance of the adsorbents in the removal of Iron. The result obtained using 0.2 M of KOH at 400 °C gave un-adsorbed Iron concentration of 0.4 mg/l, 0.3 mg/l and 0.1 mg/l for PKH, CCS and GNS respectively. Comparing these values with what was obtained at 450 °C and 500 °C, it was observed that there was a gradual increase in the amount of un-adsorbed Iron for all the adsorbents suggesting that 400 °C could be an optimum temperature for Iron removal using these adsorbents. Also, comparing the amount of un-adsorbed iron for 0.2 M and 0.1 M KOH, it was observed that adsorption of Iron using 0.1 M

KOH gave better result than 0.2 M KOH. This suggests that 0.1 M could be a better activation concentration of these adsorbents using KOH. Higher concentration of activating agent (0.2M KOH) leads to excessive activation which destroyed the internal structure of the activated carbon with part of the micropores turning into large pores resulting in a decrease in adsorption. Thus, the concentration of KOH solution has an influence on the preparation and adsorption ability of activated carbons. (Yang et al., 2017). From Figure 3(c), it was observed that the un-adsorbed Chromium concentration was 0.1 mg/l, 0.2 mg/l and 0.1 mg/l using PKH, CCS and GNS at 400 °C respectively; 0.2 mg/l for all adsorbents at 450 °C and 0.2 mg/l, 0.1 mg/l and 0.2 mg/l for PKH, CCS and GNS respectively. This suggests that PKH and GNS will perform better at 400 °C while CCS will do well at 500 °C when activated with 0.2 M KOH. Comparing the performance of these adsorbents in Chromium removal using 0.2 M KOH to that of 0.1 M KOH, it

was observed that for temperatures 400 °C, 450 °C and 500 °C when 0.2 M KOH was used, the lowest un-adsorbed Chromium concentration was 0.1 mg/l however, for 0.1 M KOH, 0.01mg/l was recorded. This suggests that KOH activation concentration of 0.1M will work better for these adsorbents than 0.2 M for similar reasons mentioned above. Figure 4(a) shows the un-adsorbed concentration of Lead. It was observed that the un-adsorbed Lead concentration for 0.2 M KOH was 0.03 mg/l, 0.04 mg/l and 0.03 mg/l at 400 °C; 0.050 mg/l, 0.050 mg/l and 0.06 mg/l at 450 °C and 0.03 mg/l, 0.06 mg/l, 0.06 mg/l at 500 °C for PKH, CCS and GNS respectively. However, when 0.1 M KOH was used, the performance at 450 °C and 500 °C seems better for all adsorbents giving a minimal un-adsorbed concentration of 0.03 mg/l (PKH) and 0.02 mg/l for CCS and GNS. Adsorbents prepared by KOH activation exhibit great advantage in Lead ion removal from aqueous solutions as also observed by Chengwen et al., (2014).

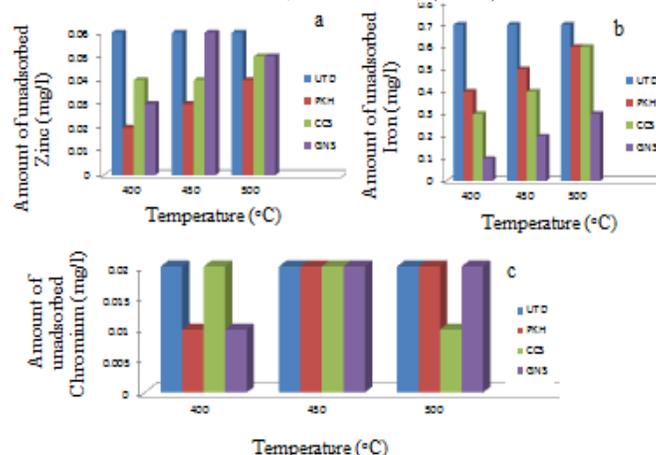


Fig 3: Amount of un-adsorbed (a) zinc (b) iron (c) chromium for 0.2 M KOH with palm kernel husk (PKH), coconut shell (CCS), groundnut shell (GNS) as adsorbent and untreated (UTD)

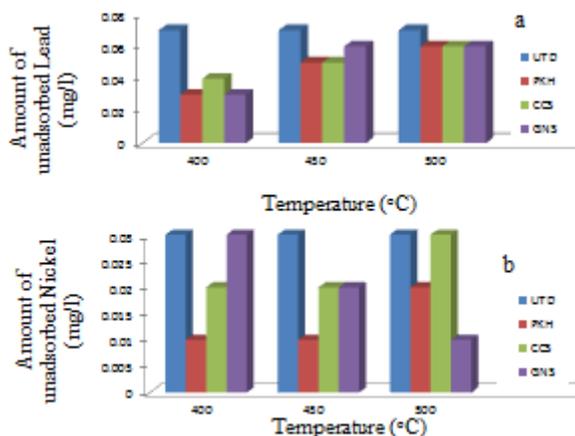


Fig 4: Amount of un-adsorbed (a) lead (b) nickel 0.2 M KOH with palm kernel husk (PKH), coconut shell (CCS), groundnut shell (GNS) as adsorbent and untreated (UTD)

Figure 4(b) then shows the un-adsorbed Nickel when the adsorbents were used at the operating temperatures. It was observed that PKH performed better at 400 °C and 450 °C while GNS was at 500 °C with 0.01 mg/l un-adsorbed Nickel concentration. Interestingly, the trend observed in this case with 0.2 M KOH seems to be very similar to that for 0.1 M KOH. This suggests that for Nickel adsorption using these adsorbents, the concentration of the activating agent (0.1M and 0.2M) may not be of serious consequence. The purpose of KOH activation is to activate the mesopores and micropores of the activated carbon. (Yang et al., 2017) However, at optimum concentration of activating agent, the adsorption capability of the adsorbents remains unchanged which implies that the optimum concentration for activating agent has been achieved.

Specifically, Figure 5(a) shows the adsorption profile for Zinc using 0.1 M ZnCl₂. At 400 °C, it was observed that PKH, CCS and GNS recorded un-adsorbed Zinc concentration of 0.01, 0.04 and 0.01mg/l respectively. Comparing this result with what was obtained when KOH was used, it was observed that the performance of the adsorbents were the same except for CCS where 0.03 was recorded for KOH. However, at 450 °C which seems to be the optimum temperature for

ZnCl₂ activation, the result seems very well better than when KOH was used and at 500 °C, there was not much observable difference in the adsorbent performance for both activating agents. This suggest that for Zinc adsorption, activating the adsorbent using Zinc chloride could be a better option as this will ensure cleaner and safer water. Figure 5(b) describes the removal of Iron using the adsorbents on activation with 0.1 M ZnCl₂ at 400 °C to 500 °C. At 500 °C, all adsorbents gave the same amount of un-adsorbed Iron while the result showed the least set of un-adsorbed Iron and the highest at 450 °C. This shows that removal of Iron by the selected adsorbents could be temperature dependent. In Figure 5(c), the removal of Chromium was described. It was observed that for all adsorbents and all temperatures, the un-adsorbed Chromium concentration was 0.01 mg/l except for 400 °C where CCS and GNS showed a poor performance and left the Chromium concentration still at 0.02 mg/l. This suggest that while Chromium adsorption could be temperature sensitive, it is more sensitive for CCS and GNS and that PKH could be better for Chromium adsorption comparing the performances of the three adsorbents. Owlad et al., (2010) reported a 12.6 mg/g adsorption capacity for Cr (VI) ion in impregnated palm shell activated carbon with polyethylenimine..

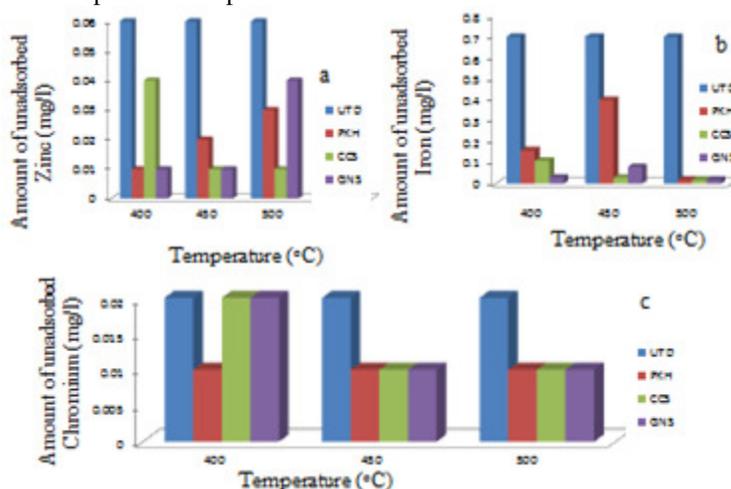


Fig 5: Amount of un-adsorbed (a) zinc (b) iron (c) chromium 0.2 M KOH with palm kernel husk (PKH), coconut shell (CCS), groundnut shell (GNS) as adsorbent and untreated (UTD)

This confirms that PKH is a good adsorbent for Chromium ion removal from waste-water. The performance of the adsorbents in Lead adsorption is presented in Figure 6(a). It is evident that the adsorbents performed well at 400 °C and 450 °C giving un-adsorbed Lead concentration of 0.01 mg/l except PKH that gave 0.02 mg/l at 450 °C. However, at 500 °C, it can be observed that the Lead concentration barely reduced to 0.03 mg/l, 0.04 mg/l and 0.04 mg/l for PKH, CCS and GNS respectively. This suggests

that at 400 °C and 450 °C, the adsorbents will perform optimally and 400 °C could be the optimal temperature for all three adsorbent since it gave the lowest un-adsorbed Lead concentration. Figure 6(b) examines the adsorption of Nickel for 0.1M ZnCl₂. It was observed that the performance of PKH and CCS improved as temperature increased while for GNS the performance was optimum at 400 °C. In all, PKH showed a better performance in all three temperatures. Finally, Figures 7 to 8 show the effect of increase in

concentration of ZnCl₂ from 0.1 M to 0.2M on the adsorption capacities of the different adsorbents. Figure 7(a) shows the performance of the adsorbents on Zinc removal. It was observed that CCS performed better making it the preferred adsorbent for Zinc

adsorption. However, comparing these performances to that of 0.1 M ZnCl₂ above, it was observed that the case with 0.1 M ZnCl₂ seems to have been better since concentrations as low as 0.1mg/l were recorded for all adsorbents at different temperatures.

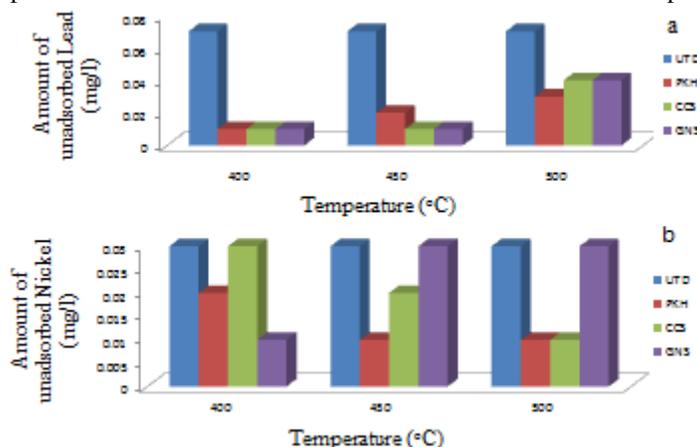


Fig 6: Concentration of un-adsorbed (a) lead (b) nickel metal using palm kernel husk (PKH), coconut shell (CCS), groundnut shell (GNS) activated with 0.1 M Zn Cl₂ as adsorbent and untreated (UTD) waste-water

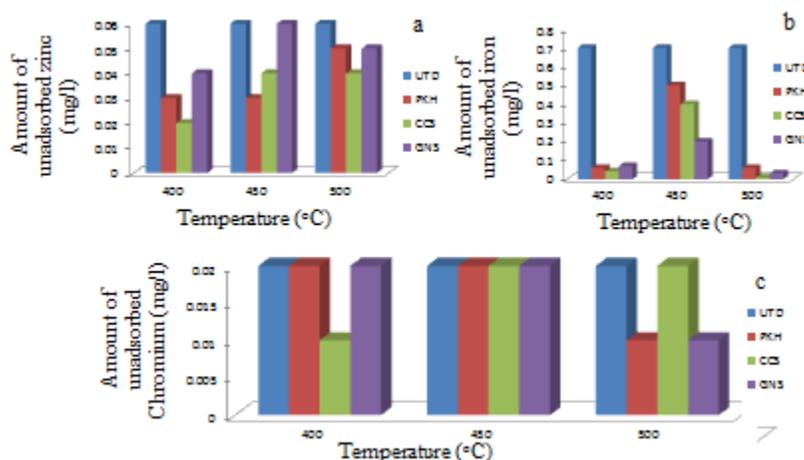


Fig 7. Concentration of un-adsorbed (a) Zn (b) Fe (c) Cr metal using PKH, CCS, and GNS activated with 0.2 M ZnCl₂ and untreated (UTD) wastewater

Figure 7(b) shows the performance of the adsorbents in the removal of Iron. PKH did not show good Iron removal capacity with activation using 0.2M ZnCl₂ as compared to the degree of Iron recovery recorded in the case of 0.1 M ZnCl₂ across all temperature used for this study. Similar observation was noted with CCS at lower temperatures. However, it gave a relatively good result at 500 °C suggesting that the performance of CCS is highly temperature dependent. GNS on the other hand gave an optimum performance at 450 °C with 0.2 mg/l of un-adsorbed Iron. This value is the same as the optimum value recorded for 0.1 M but at a different temperature. This suggests that the performance is highly temperature dependent. Figure 7(c) describes the performance of the adsorbents in the

removal of Chromium. Like the case of 0.1 M ZnCl₂, all three adsorbents showed capacity to reduce Chromium but to 50% at any stage. However, this capacity is also temperature dependent as can be seen from the figure. Figure 8(a) describes the capacity of the adsorbents to remove Lead. The results suggest that the adsorbents activated with 0.2 M ZnCl₂ have low capacity to remove lead compared to what was recorded for 0.1M irrespective of the operating temperature. Figure 8(b) describes the removal of Nickel on activation with 0.2 M ZnCl₂. The result shows that the performance is not different from what was recorded for 0.1 M ZnCl₂ but the temperatures are quite different. From Figure 7 to 8, it was observed that the activation temperature seemed to have played an

important role in the heavy metal removal. This is because temperature has been identified as an important factor which affects the sorption capacity of adsorbents. XiaBiao *et al.*, (2013) observed that increasing the calcination temperature leads to

increasing porosity and available surface area which enhance the adsorption capacity of the adsorbents. It is therefore expected that when the activation temperature increases, the heavy metal removal rate for different adsorbents will increase

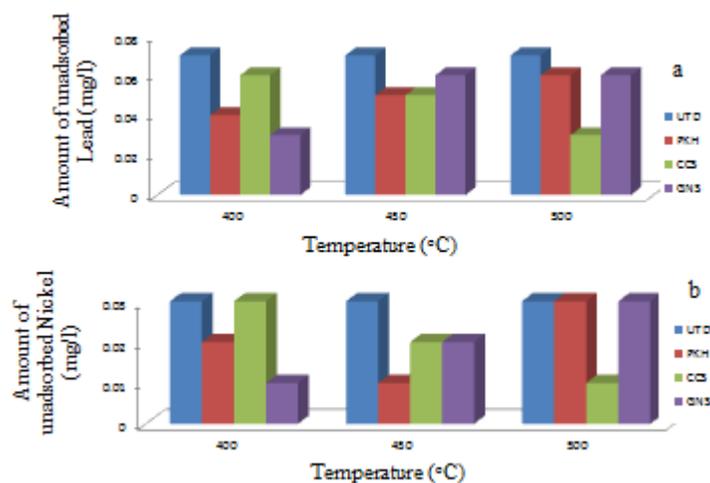


Fig 8. Concentration of un-adsorbed (a) Pb (b) Ni metal using PKH, CCS, and GNS activated with 0.2 M ZnCl₂ and untreated (UTD) wastewater

In general, CCS seems to have better adsorption capacity compared to PKH and GNS for the different temperatures and concentrations of the two activating agents. Similar conclusion was made in a recent study by Boadu *et al.*, (2018), that CCS have good physicochemical properties for adsorption and is a better advantage to be used as an adsorbent for heavy metals compared to GNS and PKH due to its good pore diameter of 2.840 nm and high BET (Brunauer-Emmett-Teller) surface area of 1177.520 m²/g an indication of the presence of many adsorption sites.

Conclusions: This work has shown that PKH, CCS and GNS could be used as alternative to available commercial adsorbents for cement waste water. It has also affirmed that the combination of physical and chemical treatment of these adsorbents could enhance their adsorption capabilities due to their resultant high surface area and increased depth of pore spaces. Within the scope of the experimental investigation, the adsorption capacities showed sensitivity to temperature, with an inverse relationship for PKH and CCS and direct relationship for GNS.

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