

Effect of the injection of pure oxygen into a membrane bioreactor on the elimination of bisphenol A

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Abstract The effect of the injection of pure oxygen instead of air in a membrane bioreactor for the elimination of bisphenol A is investigated. A dynamic experiment was developed in a pilot plant where the aerobic reactor was continuously spiked with 1 mg L^{-1} of bisphenol A. Air was injected for 10 days and then pure oxygen was injected for another 10 days. The bisphenol A concentration was determined in aqueous phases and activated sludge using simple and sensitive analytical methods based on different extraction procedures and liquid chromatography tandem mass spectrometry analysis. Enzymatic activity was also determined and toxicity tests were performed to discard that the spiked bisphenol A concentration could negatively affect the microorganisms in the bioreactor and, thus, the membrane bioreactor performance. The effluent bisphenol A concentration increased up to 0.26 mg L^{-1} after 4 days in the air injection treatment, and up to 0.48 mg L^{-1} after only 12 h in the oxygen injection treatment. In both cases, this was followed by a decrease in concentration despite the continuous spiking of bisphenol A into the bioreactor. In presence of pure oxygen, bisphenol A concentration reached background levels (below the limit of quantification) after 5 days. In contrast, when using air a total of 10 days were required to reach background levels. The

injection of pure oxygen instead of air is an important innovation in wastewater treatment, allowing permanent elimination of organic contaminants, avoiding their return to the environment and ensuring the safety of water.

Keywords Bisphenol A · Liquid chromatography tandem mass spectrometry · Membrane bioreactor · Sewage sludge · Wastewater

Introduction

Endocrine disrupting chemicals (EDCs) are known to mimic natural hormones thus causing adverse effects in humans and wildlife. Their effects lead to reduced fertility, congenital malformations of the reproductive tract and increased incidence of cancer in estrogen-responsive tissues (Bonefeld-Jørgensen et al. 2007). Recent studies focus on anthropogenic EDCs, such as synthetic hormones, a great variety of pharmaceuticals and personal care products, as well as a large amount of industrial chemicals, especially BPA, PCBs, dioxins, pesticides, phthalates, alkylphenols and alkylphenol ethoxylates (Smith 2009).

BPA is the EDC causing the greatest concern in the scientific and medical community, because its effects are even more pernicious than those caused by other EDCs. BPA can interact with estrogen receptors and is a human androgen receptor antagonist, even at low doses. It is thought that BPA can negatively affect the neuroendocrine, behavioural and cognitive functions of individuals (Takayanagi et al. 2006). In addition, BPA may also cause feminization of numerous species, inhibition of male phenotype and spermatogenesis, stimulate the growth of breast tumour cells, act as teratogenic and carcinogenic agent, and can affect the thyroid function (Furuya et al. 2006; Stowell et al. 2006). The presence of

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BPA in blood is also associated with recurrent miscarriage and development of polycystic ovary syndrome (Meeker et al. 2009).

BPA is one of the most produced chemicals in the world, with an annual production of more than 3.2 million tons (EPA 2005). It is used in the manufacture of polycarbonate plastics and epoxy resins used to line metal cans, and in many plastic products including baby bottles, toys, water pipes, drinking and food containers and other food-contact items, eyeglass lenses, dental monomers (composites and sealants) and medical equipments. The migration from food and beverage containers is considered as the primary route of human exposure to BPA. As a consequence, it can be found in biological fluids and tissues (Vandenberg et al. 2007). Environmental exposure to BPA is also a cause of concern. Wastewater containing BPA is a source of contamination of the aquatic environment (Kang et al. 2006), and low concentrations of BPA are able to cause effects if the exposure is continuous. BPA is not completely removed by currently available wastewater treatments, consequently it remains in effluents, at concentrations ranging from very low levels— ng L^{-1} (Drewes et al. 2005; Lagana et al. 2004)—to high levels— mg L^{-1} (Clara et al. 2005; Vethaak et al. 2005)—including extremely high levels in WWTP effluents from factories— mg L^{-1} (Mohapatra et al. 2010). The discharge from such effluents is the main responsible for the wide distribution and occurrence of BPA in surface waters, from 0.5 ng L^{-1} (Kuch and Ballschmiter 2001) to 1 mg L^{-1} (Vethaak et al. 2005); ground waters, up to 0.93 mg L^{-1} (Hohenblum et al. 2004); and even in drinking waters, up to 5 ng L^{-1} (Rodríguez-Mozaz et al. 2004). Incomplete removal of BPA by existing WWTPs is the result not only of the fluctuation of BPA levels in the influent, but also of the processes that take place at the WWTPs, and as well as the operational conditions.

Effluents containing BPA after landfill leachate treatment are known to be a source of BPA contamination in the aquatic environment; from groundwater enters rivers, streams and drinking waters (Nascimento Filho 2003). Evidence exists demonstrating that BPA poses a serious threat to aquatic life even at the low concentrations at which it is found in aquatic ecosystems (Talsness et al. 2009).

As the conventional activated sludge process is not capable of removing all the BPA, new treatments need to be considered to minimize the discharge of this compound. Membrane bioreactors (MBR) are a satisfactory alternative providing significant improvements over conventional treatments, like separation of treated waters by membrane filtration, which ensures the absence of solid particles and microorganisms in the effluents. MBRs are operated at higher biomass concentration, which means that the plant

can operate at longer solids retention time (SRT) facilitating additional biological transformation of micropollutants in general. While some studies exist on the fate of BPA in MBRs (Hu et al. 2007; Chen et al. 2008), there is little information about the final fate of the compound in WWTPs. Elimination of BPA from waters do not ensure its ultimate degradation because the hydrophobic properties of BPA facilitate its adsorption on the sludge and on the ultrafiltration membrane during wastewater treatment, and complete degradation is not achieved under these conditions (Spring et al. 2007). More research is required regarding the water/sludge partition ratio of BPA to develop processes that help to minimize sorption of the compound on sludge (Ivashechkin et al. 2004).

Other problem related to BPA is the generation of by-products during depuration process and improving the efficiency of the treatments has become, therefore, strictly necessary. In this respect, several studies have focused on the application of tertiary treatments, which usually include an oxidative process. These treatments are usually effective (Lenz et al. 2004; Schröder 2006) but they may result in high expenses and secondary pollution, caused by the presence of residual amounts of the oxidants or their by-products in water.

The aim of this work is to study the final fate and the main elimination pathways of BPA using the MBR technology. In addition, the work proposes an alternative to use pure oxygen instead of air to increase significantly the driving force for oxygen mass transfer for aeration and provide more oxidative conditions into the bioreactor, enhancing the degradation processes. Although aeration represents the major power input in a MBR system (about 90 % of biological treatment), this alternative becomes feasible because the use of pure oxygen can lead to a reduction in the operating costs of about 20 % in comparison with air, resulting in an oxygen positive balance, because the required energy for processes is much lower (15–20 %). In order to fulfill this objective, we carried out a dynamic experiment in a MBR pilot plant. The BPA removal efficiency was evaluated and compared in two different situations: air injection and pure oxygen injection into the bioreactor. The enzymatic activity was also tested during the whole experiment to determine the effect of air and pure oxygen on the microbiological activity in the bioreactor.

Materials and methods

Chemicals

Analytical grade standards of bisphenol A (BPA) and deuterated BPA (BPA- d_{16}), the substrates for testing

enzymatic activity and nutrient broth for toxicity tests, were purchased from Sigma-Aldrich (St. Louis, MO, USA). Chlorinated derivatives of bisphenol A (Cl-BPA, Cl₂-BPA, Cl₃-BPA, Cl₄-BPA) were synthesized in our laboratory (Vílchez et al. 2005). Stock solutions of BPA and derivatives were prepared in methanol, stored at −20 °C and prepared fresh monthly. Working standard mixtures were prepared by diluting the individual stock solution in methanol or in the initial mobile phase immediately before use. They were stored at 4 °C in dark glass bottles and prepared fresh weekly. The aqueous solutions of substrates for testing enzymatic activity, and the corresponding buffer solutions were prepared at the established concentrations, stored at 4 °C and prepared fresh weekly. LC–MS grade methanol and water—used for preparation of standards, acetone, ethyl acetate and ammonia (>25 %) were purchased from Fluka (St. Louis, MO, USA). Substrates and reagents for enzymatic activity and toxicity tests, as well as the salts for the culture media were obtained from Panreac (Barcelona, Spain). Water (18.2 MΩ cm) was purified using a Milli-Q system from Millipore (Bedford, MA, USA). Solid-phase extraction (SPE) sorbents were silica-based bonded C18 cartridges LiChrolut RP-18 (500 mg, 3 mL) from Merck (Darmstadt, Germany). Wastewater samples were filtered through a 0.45 µm cellulose acetate disk filter (Millipore) before analysis.

Instrumentation and software

Extraction procedures of sludge were performed in a Milestone (ETHOS SEL) microwave solvent extraction Labstation (Sheldon, CT, USA), operating at 2,455 MHz with a maximum delivered power of 1,000 W. The time, temperature and microwave power control were adjusted and controlled throughout the process using the easyWAVE 3 software, version 3.2.1.0. Detection and quantification of the analytes were performed using an Agilent 1200 series (Agilent Technologies Inc., Palo Alto, CA, USA) liquid chromatograph (LC) coupled “on line” to an API 2000 (Applied Biosystems, Foster City, CA, USA) triple quadrupole mass spectrometer using an atmospheric pressure chemical ionization (APCI) interface. A Gemini C₁₈ column (100 × 2.0 mm i.d., 3 µm particle size) and a C₁₈ guard column, both supplied by Phenomenex (Torrance, CA, USA) were used. For pH measurements, a Crison 2000 digital pH-meter with a combined glass-Ag/AgCl (KCl 3 M) electrode (Crison Instruments S.A, Barcelona, Spain) was used. A vortex-mixer (Yellow line, Wilmington, NC, USA); a Hettich Universal 32 centrifuge (Tuttlingen, Germany), and a Memmert oven (Schwabach, Germany) were also used. Sludge used for blank assays of enzymatic activity was autoclaved in a RAYPA autoclave (Barcelona,

Spain) and samples were incubated in a Memmert incubator (Schwabach, Germany). Absorbance of supernatants for enzymatic activity and toxicity tests was measured in an UNICAM 5625 UV/Vis spectrophotometer (ATI UNICAM, Brackley, UK). SPE was carried out in a Supelco (Madrid, Spain) vacuum manifold for 12 columns connected to a Supelco vacuum tank and to a vacuum pump. Data were analyzed by either one-way or multi-factor analysis of variance (ANOVA), using the software package Statgraphics 5.0 (STSC, Rockville, MD, USA) (Statgraphics 1982–2009) to identify significant differences between measurements. A level of 95 % ($P < 0.05$) was considered statistically significant.

Membrane bioreactor pilot plant description and operational conditions

The MBR pilot plant used in the experiments (Fig. 1) was provided by Air Liquide España from Zenon S.A. The MBR pilot plant has a sidestream configuration and consisted of a cylindrical bioreactor with an operational volume of 385 L into which air or pure oxygen is applied; and a rectangular bioreactor of 89 L, where two polyvinylidene difluoride (PVDF) hollow fibre membrane modules (Zenon®), with an effective area of 1.86 m² and a nominal pore size of 0.04 µm (ZW-10 Zenon®) were installed. Control devices to monitor membrane pressure, temperature of the activated sludge, suspension solids and dissolved oxygen (DO) were also available. The MBR was operated using urban wastewater from the primary settling tank of the wastewater treatment plant (WWTP) located in the city of Granada (Spain). Table 1 summarizes the operational conditions of the pilot plant for the experiments.

The characteristics of wastewater were analyzed daily during the whole experiment. The average values for each parameter used to feed the bioreactor were: 330 mg L^{−1} total chemical oxygen demand (COD), 360 mg L^{−1} biochemical oxygen demand at 5 days (BOD₅), 80 mg total N L^{−1}. Removal was around 90 % for total COD and for nitrogen, when pure oxygen was used as source of aerobic conditions in the bioreactor. The elimination performance was 97 % for suspended solids. The bioreactor was started up with no previous inoculation; thus, the microorganisms in the sludge came from the influent wastewater. Air or pure oxygen was applied into the cylindrical bioreactor to provide suitable aerobic conditions for the biological processes that will take place. DO was within the range of 2–4 mg L^{−1}. In the rectangular bioreactor, aeration was applied to create turbulence and delaying membrane fouling. The biomembrane process uses a vacuum system to pull the wastewater through the membrane that is then stored in a third tank (25 L). The flow is reversed regularly for turbulence



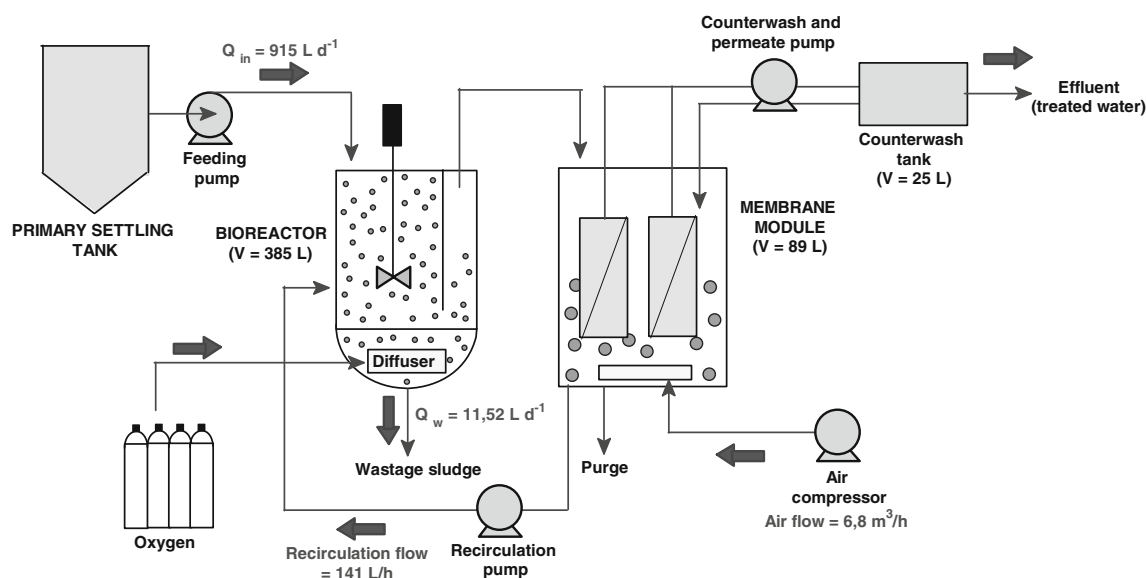


Fig. 1 Schematic diagram and picture of the MBR pilot plant including dimensions and typical flow rates

Table 1 Operational and physicochemical parameters of the MBR pilot plant during the experiments

Parameter	Influent	Effluent
Physicochemical parameters of influent and effluent water of the MBR pilot plant ^a		
pH	7.6	7.5
Conductivity ($\mu\text{S cm}^{-1}$)	1,419	1,016
COD (mg L^{-1})	330.0	30.6
BOD ₅ (mg L^{-1})	359.8	26.4
MLSS (mg L^{-1})	120.3	2.8
Total nitrogen (mg L^{-1})	80.0	7.6
MLVSS (mg L^{-1})	105.0	2.5
Parameter	Unit	Value
Operational conditions of the MBR pilot plant		
Influent flow rate	Q_{in} (L day^{-1})	915.6
Wastage sludge flow rate	Q_{w} (L day^{-1})	11.52
Hydraulic retention time	HRT (day)	0.5
Sludge retention time	SRT (day)	32
Aeration (oxygen flow)	g h^{-1}	500
Membrane module aeration	$\text{m}^3 \text{h}^{-1}$	6.8
Recirculation flow	L h^{-1}	141
	Experiment 1 (with air)	Experiment 2 (with pure oxygen)
Physicochemical parameters of the bioreactor for each experimental period ^a		
pH	7.02	6.98
Temperature ($^{\circ}\text{C}$)	23.8	27.3
MLSS (mg L^{-1})	9,300	8,500
MLVSS (mg L^{-1})	8,000	7,500
Conductivity ($\mu\text{S cm}^{-1}$)	1,156	1,063
Dissolved oxygen (mg L^{-1})	2.09	3.06
Oxidation–reduction potential (mV)	+155.6	+227.3

^a It was reported the mean value for each 10 days examination period

promotion, which allows passing treated water through the membrane in the reverse direction. This contributes to the cleaning of the membrane surface and avoids increase in transmembrane pressure (TMP) value, which is an indicator of the degree of membrane fouling. Plant operation consisted of 10-min cycles: a filtration cycle lasting 9 min 45 s followed by a back flush cycle lasting 15 s. A system for the purge of excess sludge was also provided.

Experimental protocol

The bioreactor was continuously spiked with 893 mg of BPA per day, equivalent to a total influent BPA concentration of 1 mg L^{-1} . This concentration was selected based on a previous study (Lindblom et al. 2009) to evaluate the MBR capability for BPA removal from waters under conditions of high pollution levels of this contaminant. In order to establish differences between the use of air and pure oxygen to provide aerobic conditions in the bioreactor, two experiments were performed during spring 2010, with a mean temperature inside the bioreactor of 26°C . The experimental work in the plant was divided in two consecutive stages: the first experiment was performed during 10 days and involved the use of air from a compressor as source of oxygen for the bioreactor. Once the first experiment was completed, the second one was immediately initiated, involving the use of pure oxygen during other 10 days. The mean values for the physico-chemical parameters measured in the bioreactor during the two 10-day experiments are presented in Table 1. During both experiments, samples of influent, effluent water and sewage sludge were collected at defined time intervals to determine BPA concentration. Samples from the bioreactor mixed liquor were also taken for the analysis of the enzymatic activity of the bacterial populations living in the bioreactor. Before the spiking of the bioreactor with BPA, samples of the bioreactor mixed liquor were taken for the corresponding toxicity tests.

Sample collection and analysis

Sampling and extraction of samples for EDCs determination

All water and sewage sludge samples were collected and stored in amber glass bottles. Immediately after the sampling, decreased biological activity was achieved by addition of 1 % (v/v) aqueous formaldehyde. Once in the laboratory, water samples were centrifuged, filtered and stored in the dark at 4°C , until analysis. Sludge samples were also centrifuged and the solid fraction was recovered, dried in a heater at 60°C to constant weight and finely

ground ($\leq 1.41 \text{ mm}$). The samples were kept in the dark at 4°C until analysis. Both types of samples were processed within the allowable holding period. The determination of BPA concentration in water samples was performed according to a method described elsewhere (Zafra-Gómez et al. 2008) with some modifications. Briefly, BPA was extracted from samples using a SPE procedure with LiChrolut RP-18 cartridges. 100 mL of wastewater was passed through the cartridges and after extraction; the analytes were eluted with a mixture of diethyl ether–methanol (90:10; v/v). Eluents were evaporated to dryness at 50°C under a stream of nitrogen. The residues were re-dissolved in 500 μL of the initial mobile phase and directly injected into the LC system. The determination of sorbed BPA in sludge samples was performed using a modified analytical method that was adapted for sludge samples (Liu et al. 2004). Briefly, Sludge sample (1.0 g) was placed in a microwave Teflon vessel with 10 mL of ethyl acetate as extraction solvent. The suspensions were extracted for 10 min (10 min for holding) at 90°C and at 1,000 W. After microwave irradiation, the vessels were allowed to air-cool inside the microwave to below 45°C . The extract was centrifuged for 35 min at $3,634\times g$ and evaporated to dryness at 50°C under a stream of nitrogen. The residue was resuspended with 500 μL of the initial mobile phase, centrifuged at $3,634\times g$ for 10 min and the supernatant was directly injected into the LC system. To study the efficiency of the extraction procedures, a recovery assay was carried out. Water and sludge samples were spiked in triplicate with a standard solution of compounds ($1 \mu\text{g L}^{-1}$ for wastewater and $200 \mu\text{g kg}^{-1}$ for sludge samples). Spiked samples and a blank sample were analyzed and the recoveries of the analytes were above 96 and 94 % on average for wastewater and sludge, respectively. The limit of quantification (LOQ) of the method was calculated on the basis of a signal-to-noise ratio (S/N) of 10. For BPA, the LOQ was 52 ng L^{-1} in wastewater and $18 \mu\text{g kg}^{-1}$ in sludge. For the derivatives, the LOQ was between $24\text{--}43 \text{ ng L}^{-1}$ for wastewater and $20\text{--}30 \mu\text{g kg}^{-1}$ for sludge.

LC–MS/MS analysis

A Gemini C_{18} column ($100 \times 2.0 \text{ mm i.d.}$, $3 \mu\text{m}$ particle size) and a C_{18} guard column were used for LC analysis. The flow rate was $350 \mu\text{L min}^{-1}$, the column was maintained at 40°C , and the injection volume was $40 \mu\text{L}$. The standards and samples were separated using a mobile phase consisting of 0.025 % (v/v) ammoniacal aqueous solution and 0.025 % (v/v) ammonia in methanol, with a methanol gradient from 60 to 100 % in 5 min. Multiple reaction monitoring (MRM) was used. APCI was performed in the negative ion mode. The mass spectrometric conditions



were as follows: ion source temperature, 350 °C; IonSpray voltage, −3 kV, nitrogen was used as both the curtain gas at 30 psi and ion source gas 1 and 2 at 50 and 30 psi, respectively; collision gas was air at 10 psi. To optimize MRM conditions, a full scan and a product ion spectrum for each compound were first acquired by infusion of standard solutions of each analyte. Declustering potential, focusing potential, entrance potential, collision energy, and collision cell exit potential were optimized to obtain the maximum sensitivity with the highest amount of product ions available. Two pairs of Q1/Q3 were chosen for each compound, except for the surrogate, because it was an isotopically labelled compound that is unlikely to be found in environmental samples (BPA: 227.2, 212.2/132.9; Cl-BPA: 261.1, 182.1/210.0; Cl₂-BPA: 295.1, 244.1/215.2; Cl₃-BPA: 329.1, 250.1/278.0; Cl₄-BPA: 365.0, 314.2/286.1; BPA-d₁₆: 241.2, 142).

Determination of enzymatic activities

The samples for the determination of enzymatic activity were collected in sterile plastic containers and immediately transported to the laboratory at 4 °C. The determinations were performed no later than 8 h after sampling. The activity of six enzymes was determined: alkaline and acid phosphatase (Goel et al. 1998), α -glucosidase (Goel et al. 1998), esterase (Boczar et al. 2001), protease (Cadoret et al. 2002) and dehydrogenase (Awong et al. 1985). All enzyme assays were based on colorimetric methods, and are described in literature. Enzymatic activity was expressed as mM min^{−1} g MLVSS^{−1}.

Determination of physicochemical parameters

The concentration of mixed liquor suspended solids (MLSS), mixed liquor volatile suspended solids (MLVSS), COD, BOD₅, and total nitrogen were determined by standard methods (APHA 2001). Temperature, pH, DO, oxidation–reduction potential, and conductivity were determined by specific sensor electrodes (Crison Instruments).

Toxicity tests

Growth inhibition of activated sludge The information obtained from this test is helpful for choosing suitable BPA spiking concentration, in other words, a concentration that will not cause toxic effects to microorganisms in sludge reducing their ability to degrade the evaluated substances. The growth inhibitory effect of BPA on activated sludge microorganisms was performed in accordance with the ISO 1995 guideline (Strotmann and Pagga 1996). Flasks containing organic test medium and test substance were

inoculated with an overnight culture of mixed sewage microorganisms and incubated at 22 ± 2 °C for up to 6 h. The test was completed when the exponential growth in the controls ceased. The bacterial biomass was quantified as turbidity in both control and test vessels spectrophotometrically at DO 530 nm. Results were reported as the effect concentration to 50 % inhibition (EC₅₀), which were obtained by interpolation from the obtained inhibition curve using ten concentration levels.

Calculations

Removal efficiency of BPA was calculated by a mass balance in each experiment, using the obtained data of concentrations in water and sorbed on sewage sludge (Stasinakis et al. 2007). After calculating the biodegraded BPA mass, the biotransformation rates were determined, assuming a pseudo–first–order degradation kinetic (Clara et al. 2005). The solid–water distribution coefficients (K_d) were calculated to analyze the amount of BPA sorbed on sludge in the MBR process during both treatments (Wu et al. 2011).

Results and discussion

During the experiments, no BPA concentrations above the LOD of the method were found in influent wastewater, but at the beginning of the experiments, 680 µg kg^{−1} of sorbed BPA was detected in the activated sludge.

Effect of spiked BPA on the growth of microorganisms in the bioreactor

From the inhibition curve, it was determined that BPA caused growth inhibition at very high concentrations (EC₅₀ = 29.4 mg L^{−1}). It was observed that concentrations <1 mg L^{−1} did not cause any noticeable acute toxic effects on the microorganisms in the bioreactor. The slight acute toxicity of BPA on bacteria is supported by some previously published studies (Groshart and Okkerman 2001; Zhang et al. 2007). Therefore, the working concentrations of BPA had no acute toxic effects and did not interfere with the biological activity in the bioreactor.

Comparison of BPA removal between the two treatments

The response to the treatments with air and pure oxygen, in relation to the elimination of the spiked BPA in the bioreactor, is shown in Fig. 2a, b. In both treatments, the

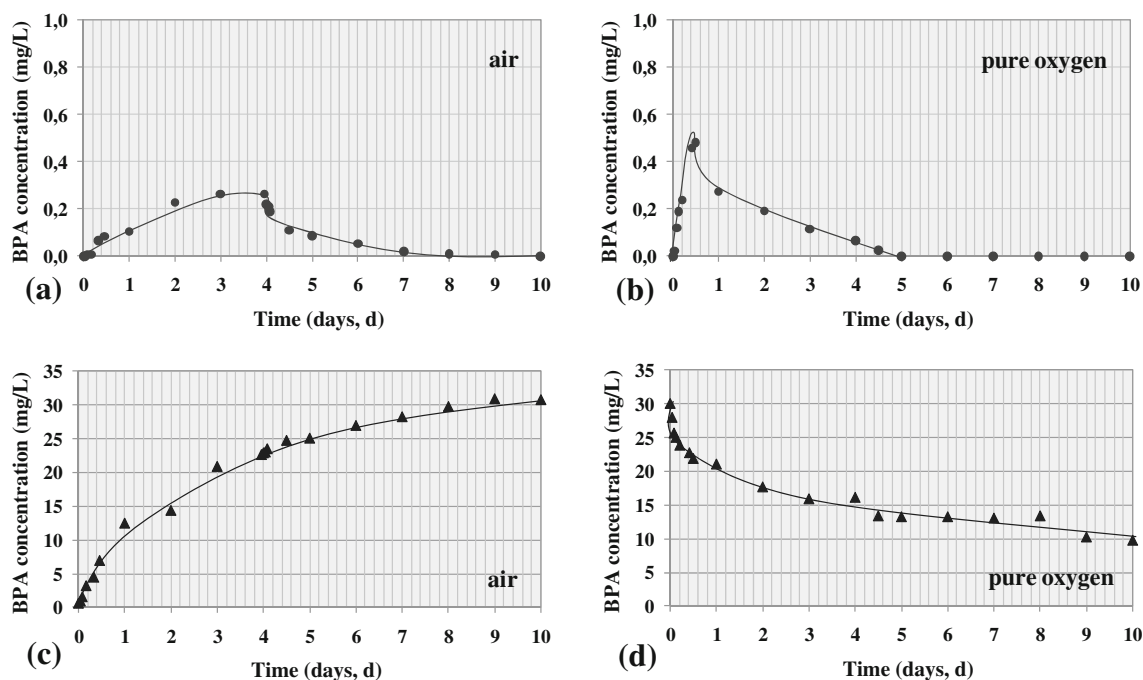


Fig. 2 Measured curves for BPA during each experimentation period with air and pure oxygen. **a, b** Evolution of effluent BPA concentrations; **c, d** evolution of sorbed BPA concentrations to activated sludge in the bioreactor

measured effluent BPA concentrations did not converge eventually towards the spiked influent concentration, as it could be expected. The highest BPA concentrations in the effluent were 0.26 and 0.48 mg L⁻¹ for air and oxygen, respectively. The results constitute evidence that removal processes in the fast dynamic region, like sorption, contribute significantly to the fate of BPA, as Fig. 2 shows. Subsequently, as the experiment progresses, the removal of BPA increased until the measured concentrations in effluent reached the background BPA level, which was below the LOD of the method. In presence of oxygen, BPA concentrations in the effluents reached the background level only after 5 days, which was faster than in the case of the treatment with air, where spiked BPA concentration after 5 days was about 9 % and 10 days were required for reaching the background level.

Distribution of BPA in the MBR system

Mass balances were performed for both experiments. For the calculations, it was assumed that the main routes for the elimination of BPA from water were only biodegradation and sorption to sludge, since it is known that no other transformation pathways are possible. BPA is a non-volatile compound and tends to sorb to soil. On the other hand, the physical and chemical properties of BPA suggest that hydrolysis is likely to be negligible (UK-BRE 2000). Furthermore, although BPA has the potential to photolyze in

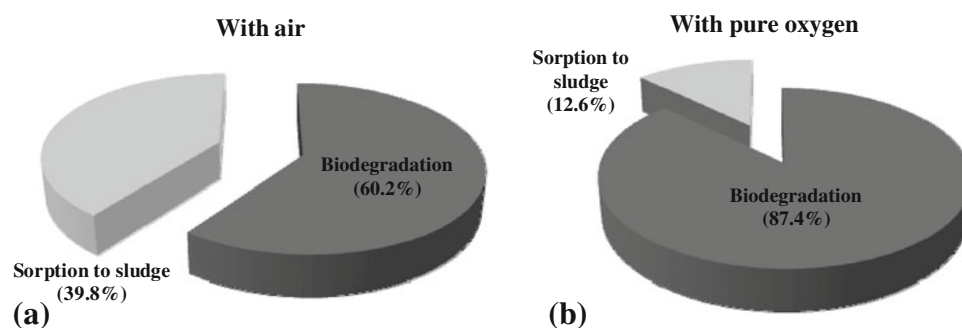
water, this is not a probable mechanism in activated sludge systems, where the presence of humic acids compete in absorbing photons protecting BPA from an effective photodegradation, causing a shielding effect (Schmitt-Kopplin et al. 1999). Steady-state conditions were assumed when effluent concentrations stabilized around the background concentrations after each experiment. As a result of mass balances in the bioreactor, it was obtained the whereabouts of BPA treated under MBR conditions. The results are presented in Fig. 3.

Influence of biodegradation and study of enzymatic activities

It could be concluded that biodegradation was the main elimination pathway for BPA, which is responsible for the return to a new steady-state effluent concentration in both treatments, even though BPA was continuously being spiked into the bioreactor. Biodegradation rate also increases over time with both air and oxygen, and it is logical to assume that the biomass capable of degrading BPA in the system also increases. The simplest explanation is the growth of specific heterotrophic organisms of activated sludge. A large part of BPA was rapidly biodegraded (about 44 %) during the first day of BPA spiking into the bioreactor, suggesting that the enzymes required for BPA biodegradation were already present. Over the following days of the experiment, biomass acclimatization to BPA



Fig. 3 Mass flow chart demonstrating the fate of BPA during the two treatments



resulted in a gradual increase of its biodegradation potential. These observations are consistent with the assumption that such degraders are naturally present in the activated sludge, growing under aerobic conditions, since no biological degradation is observed during anoxic or anaerobic conditions (Chen et al. 2008; Schröder 2006; Press-Kristensen et al. 2008). This work has proved that the source of oxygen is of crucial importance in the final fate of BPA. The change from air (traditional source of oxygen) to pure oxygen improved the biodegradation and sorption mechanisms. The use of pure oxygen increased the biodegradation percentages from 60.2 % (air) to 87.4 % after a 10-day period of exposure. The biotransformation rates also confirm this behaviour, since k_{obs} value was higher for the treatment with oxygen ($0.23 \text{ L g X}_{\text{MLVSS}}^{-1} \text{ day}^{-1}$) than for the treatment with air ($0.15 \text{ L g X}_{\text{MLVSS}}^{-1} \text{ day}^{-1}$). Moreover, with pure oxygen the biodegraded mass of BPA per day increased over time since day 2 and more rapidly than in the presence of air, where the biodegradation rates increased significantly from day 4. Eventually, biodegradation rates reached a background level in both cases. The study of activities showed the changes that bacterial enzymes underwent during both treatments (Fig. 4).

It was observed that the change from air to oxygen had a clear impact on the activity of certain enzymes in activated sludge, since other important parameters that could determine this behaviour, such as MLVSS, pH and temperature were approximately constant during both treatments. The composition of the inlet (raw wastewater) is a very difficult to control parameter because of its complexity; however, considering the relatively short duration of the experiments and its permanent urban nature, the influence of the inlet was not considered. Acid and alkaline phosphatases, dehydrogenases, and α -glucosidases increased rapidly and significantly their activity as a result of the change to pure oxygen, which could explain the increase in the biodegradative potential of microorganisms in the bioreactor. This study corroborates the importance of the dehydrogenase enzyme as indicator of biological activity, since some studies have proved good correlations between dehydro-

genase activity and other indicators of sludge viability like oxygen uptake rate (Awong et al. 1985). For this reason, this enzyme assay is considered an indicator of activity in activated sludge (Awong et al. 1985; Dutton et al. 1983). Moreover, this study provides clear evidence that other enzymes, like acid and alkaline phosphatases and α -glucosidase, are also indicators of the bacterial activity into the bioreactor. Dehydrogenase and α -glucosidase exhibited an increase in their activity of about 100 % as a result of the change from air to oxygen, whereas acid (83 %) and alkaline (61 %) phosphatases also showed significant but lower increases. These enzymes are, therefore, good indicators of microbial metabolic activity of activated sludge. Lastly, protease and esterase did not show significant changes during both treatments. The degradative activity of these enzymes is related to their hydrolytic activity which is mainly associated with the cell or lies within the extracellular polymers (ECP) of the flock. ECP could indeed hold and keep a large pool of extracellular enzymes (Goel et al. 1998), and centralized the biological activity in this place.

Influence of sorption to sludge

BPA has a relatively high octanol–water partition coefficient ($\log K_{\text{ow}} = 2.2\text{--}3.8$) (Staples et al. 1998), which is characteristic for hydrophobic compounds. This is associated with poor hydrosolubility and high tendency to sorb on organic material of the sludge matrix (Stangroom et al. 2000), and suggests that sorption may be an effective mechanism, in addition to biodegradation, for the elimination of BPA from waters. According to our results, in presence of air (Fig. 2c), sorbed BPA tends to remain accumulated in sludge, making it less available to be degraded and persistent. Usually, sludge undergoes various treatments to reduce the sorbed contaminants such as anaerobic digestion, chemical treatment and composting. However, it is known that these procedures are not effective, and contaminants persist in the environment for long



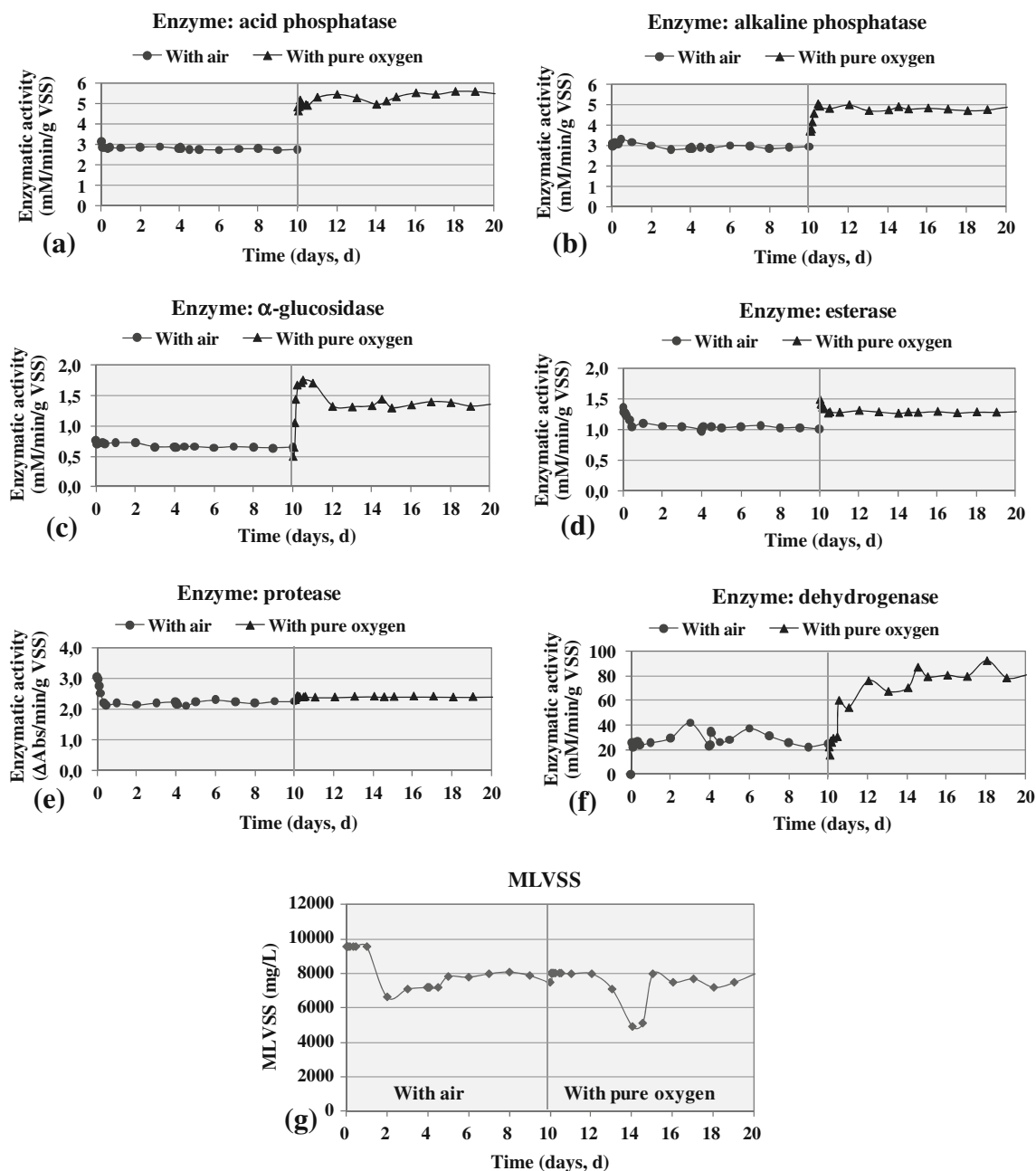


Fig. 4 Evolution curves for enzymatic activities (a–f) during the experimentation period for both treatments (with air and pure oxygen).
g Evolution curve for MLVSS during the experimentation time

periods of time. It was observed that oxygen stimulated not only biodegradation, but also favoured BPA desorption from sewage sludge (Fig. 2d). During the treatment with air, 30 mg kg⁻¹ of BPA was sorbed to sludge, which began to be gradually desorbed 3 h after the beginning of treatment with oxygen. Desorbed BPA was transferred to water, which could explain the increase in BPA concentration in the effluents at the beginning of the treatment with oxygen. It was calculated that 67.4 % of the BPA bound to sludge

underwent desorption, which was almost entirely biodegraded once it passed to water system. The differences in the sorption capacity of BPA to sludge were also demonstrated by the calculation of the solid-water distribution coefficients (K_d) for both treatments (4,574 L kg-SS⁻¹ and 508 L kg-SS⁻¹ for air and pure oxygen, respectively). The K_d value, in the order of thousands, for the treatment with air indicated a high tendency of BPA to partition onto the sludge. This behaviour changed dramatically with the use



of pure oxygen, which diminished the sorption tendency of BPA to sludge and favoured desorption process.

Effect of application of pure oxygen into the bioreactor

Based on studies that establish that BPA degradation requires aerobic conditions (Mohapatra et al. 2010), the novelty of our study is the use of pure oxygen instead of air to improve its permanent removal from wastewaters and sludge. A very distinct difference between both treatments is the significant increase in the enzymatic activity responsible for the biodegradation processes in sludge. These activities contribute to rupture and partially solubilise suspended solids, less complex molecules, including many organic contaminants, increase the soluble COD, decrease viscosity and improve the overall biodegradability (Verma et al. 2007). This could explain the positive effect of the application of pure oxygen on BPA biodegradation in the MBR. Nonetheless, further research is needed to achieve a complete understanding of the effect of pure oxygen on biological processes, especially on enzymatic activities. Some of them are significantly influenced by the redox state of the system, whereas others like protease and esterase are not apparently affected, although they play a crucial role in the hydrolysis of relevant macromolecules and many contaminants. Likewise, further research is needed to determine the effect of oxygen on sorption/desorption equilibrium. Finally, this procedure has demonstrated to be environmentally friendly because it avoids the application of a tertiary oxidative treatment that usually causes secondary pollution (Lenz et al. 2004). Moreover, the economical balance is positive despite the higher cost of pure oxygen because the use of oxygen also reduces sludge production, which means lower operating time and lower electricity consumption.

Conclusion

The injection of pure oxygen instead of air into the bioreactor of a MBR pilot plant is relevant innovation for wastewater treatment, allowing the permanent elimination of BPA by increasing the microbial activity inside the bioreactor, which results in an increase of the biodegradation rates of BPA. Likewise, application of pure oxygen facilitated desorption of BPA from sludge, which was subsequently biodegraded. Further studies are required to completely understand the mechanisms and processes involved in the positive effects of pure oxygen. It would also be interesting to study this effect on other emerging organic microcontaminants, which are a serious threat to ecosystems. The successful application of this innovation in the MBR technology could guarantee the permanent

elimination of these substances, avoiding their return to environment and ensuring the safety of treated water.

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