

# Reduction of emissions and fuel consumption in a compression ignition engine using nanoparticles

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**Abstract** In this paper, the effect of adding nanoparticles on the performance characteristics of diesel engine was investigated. Up to now, several metallic nanoadditives including cerium and aluminum have been applied in this area. However, the possibility of using some other metals or modification in the additive structures as well as improving or changing the basic fluid is among factors manifesting a broad scope of work in this area. For this purpose, the silver nanoparticles were used as additives to the net diesel fuel. The results are indicative of significant alteration in the engine power, oil temperature, and the proportion of the released pollutants. The presence of the metallic nanoparticles inside the combustion chamber augments the heat transfer to fuel and shortens the ignition delay through an acceleration of the burning process. Meanwhile, these particles can aid fuel particles further penetrate in the compressed air during the spraying stage. Having all of these features altogether will improve combustion and hence the unburned carbons and other pollutants will decrease. Based on these observations, the rate of CO and NO<sub>x</sub> would be reduced significantly up to 20.5 and 13 %, respectively, noting that the net diesel and HC would undergo the highest change (up to 28 %). The results also indicate a 3 % fuel consumption reduction accompanied with 6 % improvement in the engine power, utilizing nanoparticles in most cases.

**Keywords** Emissions · Fuel · Diesel · Engine · Nanoparticle · Additive

## Introduction

One of the most important issues raised in the automotive industry is the reduction in the fuel consumption and the pollutants from the combustion in the internal combustion engines. Previous works implemented in this field include changing the engine design, improving the quality of fuel, applying techniques on the exhaust gas and especially employing emulsification, and additives/fuel supplements (Bertola et al. 2003; Harbach and Agosta, 1991; Jung et al. 2005; Satge De Caro et al. 2001; Xiaolu et al. 2006). Additives even at the microscale have limitations and problems dealing with sedimentation, conglomeration, and nonuniform distribution. With the advent of nanotechnology in recent years, the aforementioned problems were largely resolved and considerable conclusions were made that will be dealt with subsequently.

Application of nanoparticles in fuel and the study of combustion process considering nanoparticles effect were initially reported in solid fuels and propulsion engines (Galfetti et al. 2007). According to the research conducted in 1997 by Ivanov and Tepper (1997), aluminum nanoparticles could increase the burning rate of the charge in comparison with microparticles. Furthermore, nanoparticles application in fuel demonstrated shorter ignition delay in combustion process when compared to that of microparticles (Pivkina et al. 2004). Moreover, nanoparticles featuring high surface area to volume ratio lead to more contact area between fuel and oxidizer (De Luca et al. 2005). According to the researches carried out in 2004, addition of aluminum nanopowder to the rocket fuel will

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increase the combustion efficiency (Evans et al. 2004). In another research (Kuo et al. 2004), it was revealed that Boron nanoparticles have high potential in the burning rate of solid propellants due to the existence of high heat content of combustion and more heat release rate. Hence, these nanoparticles can dynamically boost the combustion process through reducing the ignition delay, the burning time, and increasing the momentum density which in its own turn can improve the fuel's injection velocity into the combustion chamber.

In other research (Yetter et al. 2009), the interaction between metallic particles and nanotechnology in combustion phase was investigated. In addition, the combustion behavior of some metals was studied, wherein the combustion regimes of the metal particles were analyzed. This research also covers the combustion behavior of the aluminum nanoparticles. According to their work, the application of nanoparticles in the combustion systems is classified into five cases, namely: nanofluids, gels, solid propellants, solid fuels, and thermites.

In recent years, the application of nanoparticles in the combustion systems including liquid and hydrocarbon fuels drew the attention of the researchers. It was demonstrated (Tyagi et al. 2008) that the possibility of the ignition of diesel fuel with aluminum nanoparticles is much higher than the pure diesel fuel. Based on the performed tests (Gan and Qiao 2011) on the micro/nano-scaled particles of aluminum with the ethanol and *n*-decane-based fuels in the chamber with quartz windows, the rate of agglomeration of the nanoparticles is less than the micron scale agglomeration rate. The nanoparticles burning will continue up to fifth stage, while the process for the microparticles will stop at the third stage. Moreover, in another research (Gan et al. 2012) on the nano fluid fuels, it was revealed that nanoparticles exhibit two different combustion patterns when treated in the dilute and dense concentrations. By experiments on the Al (aluminum) nanoparticles and liquid fuel using an aerosol rapid compression machine, a reduction of 32–50 % in the ignition delay process was noticed (Allen et al. 2011). The effects of the Al nanoparticles and Al<sub>2</sub>O<sub>3</sub> on the heat release rate of the bioethanol fuel were studied (Li 2011), where a linear increase in the heat release was observed with the Al and decrementation of Al<sub>2</sub>O<sub>3</sub>. Some of the core and shell combinations of the nanoparticles could be used as a core with high combustion energy and a shell with catalyst property. This method was employed on Boron nanopowder (Van Devener et al. 2009) and a new type of fuel introduced with high energy density and catalyst properties. Few researches were performed practically on the diesel engine in the laboratory in terms of exploring the effect of nanoparticles on the engine per-

formance and emissions. However, a research conducted in 2012 indicates a simultaneous reduction in NO<sub>x</sub> and soot when using a catalyst containing nanoparticles (Wang et al. 2012). More recently, with adding an organic nanoparticle to the fuel, a reduction of 30.6 % of NO<sub>x</sub> and an increase of 14.2 % of the brake thermal efficiency (BTE) were reported (Yang et al. 2013). In a research performed on a diesel engine by applying aluminum nanoparticles (Kao et al. 2008), the smoke rate was reduced in revolutions of 1,200, 1,800, and 2,400 rpm, while NO<sub>x</sub> and BSFC (brake specific fuel consumption) increment was reported in revolutions less than 1,800 rpm. Also, experiments on the performance and the emissions of the diesel engines using a mixture of the diesel fuel and carbon nanotubes revealed a new trend of an increase in the BTE along with the reduction in NO<sub>x</sub>, CO, and HC (Basha and Anand 2010). An investigation carried out in 2009 (Selvan et al. 2009) represents that smoke was absorbed by nanoparticles, and the amount of CO, HC, SFC (specific fuel consumption), and heat release rate was decreased in pressures more than 0.4 MPa when cerium nanoparticles on the diesel fuel were employed on a four-stroke single-cylinder diesel engine. They also reported a reduction in the HC and the heat release rate and an increase in the BTE in pressures higher than 0.2 MPa when nanoparticles were employed in the mixture of diesel–biodiesel–ethanol. In another test (Sajith et al. 2010) implemented on the Jatropa biodiesel, a 30 % reduction in NO<sub>x</sub>, 25–40 % reduction in HC, together with 1.5 % increase in efficiency were acquired. A study in 2011 (Basha and Anand 2011), by making emulsion of water–diesel with alumin, registers a reduction of 11–25 ppm for HC, 300–395 ppm for NO<sub>x</sub>, a reduction in the heat release rate, and a reduction in the smoke opacity percentage as much as 20–35 % along with 28.8 % increase in efficiency. By implementation of the experiments on CO emission, a 6 % reduction in CO concentration has been witnessed during tests with Al<sub>2</sub>O<sub>3</sub> nanoparticles (Solero 2012).

In order to have a global outlook over physical and chemical properties of nanoparticle combustion with reference to the past experimental works, it was noticed that adopting metal powder as an additive has been long considered as a novel methodology by many researchers (William 1997). However, since a restricted number of investigations (both qualitatively and quantitatively) were performed in this area, also to survey the impact of new metals as nanoparticles on diesel engine, authors are motivated to undertake the current study. In this regard, the effect of silver nanoparticles on the diesel fuel has been investigated in this paper. This research was conducted at nanotechnology laboratories of Tehran and Urmia Uni-



versities and also at Bioenergy Research Center of Tarbiat Modarres University in May 2013.

## Materials and methods

To prepare the fuel and nanoparticle combination, first the silver powder which was made in the US Nano American company was selected in the range of 30–50 nm dimensions. Also, the sorbitan monooleate surfactant made by Sigma-Aldrich was used for the stability of nanoparticles in the diesel fuel. After only 2 % per volume of the surfactant was solved in the diesel fuel by the homogenizer, silver nanoparticles were added and afterward the prepared mixture was placed for 10 min in the ultrasonic UP400 s that was constructed by Germany's Heilscher company. Three types of fuel combinations were prepared for the experiment. Firstly, a mixture of the fuel and 10 ppm nanoparticle was made and then in the same manner a mixture of fuel and 20 ppm nanoparticle was obtained and finally a mixture of fuel and 40 ppm nanoparticle was prepared. Three types of fuel mixture in the above-mentioned procedure were denoted by D10, D20, and D40 in the diagrams accordingly. The type of engine in this experiment is a compression ignition engine with the given features in Table 1. The FTO flow meter made by an American Flowtech company was employed to measure the fuel flow with measurement range between 37 and 1,514 milliliter per minute. Flow meter operates based on a turbine with the magnetic sensor method. To conduct the experiments and control the speed and load, the Sigma 5 dynamometer (made by the English NJ-Froment company) was used. The given power in the graph is written based on the dynamometer printout. The standard power take off (PTO) speed with 6-gear shaft is 540 rpm in the engine speed of 1,893 and with 21-gear shaft is 1,000 rpm in 1,900 engine speed. In other words, the engine RPM to PTO shaft ratio by 6-gear shaft is 3.51:1 and by 21-gear shaft is 1.9:1. Concerning the MF-399 engine, a 21-gear and 1,000 rpm mode has priority due to its empowerment shaft specification; therefore, the 21-gear interface shaft was chosen.

Emission analyzer (made in Germany), which was used in this experiment, is capable of measuring the amount of outflow pollutants such as O<sub>2</sub>, HC, NO<sub>x</sub>, CO, CO<sub>2</sub> exhaust products components from the exhaust and represents the oil temperature.

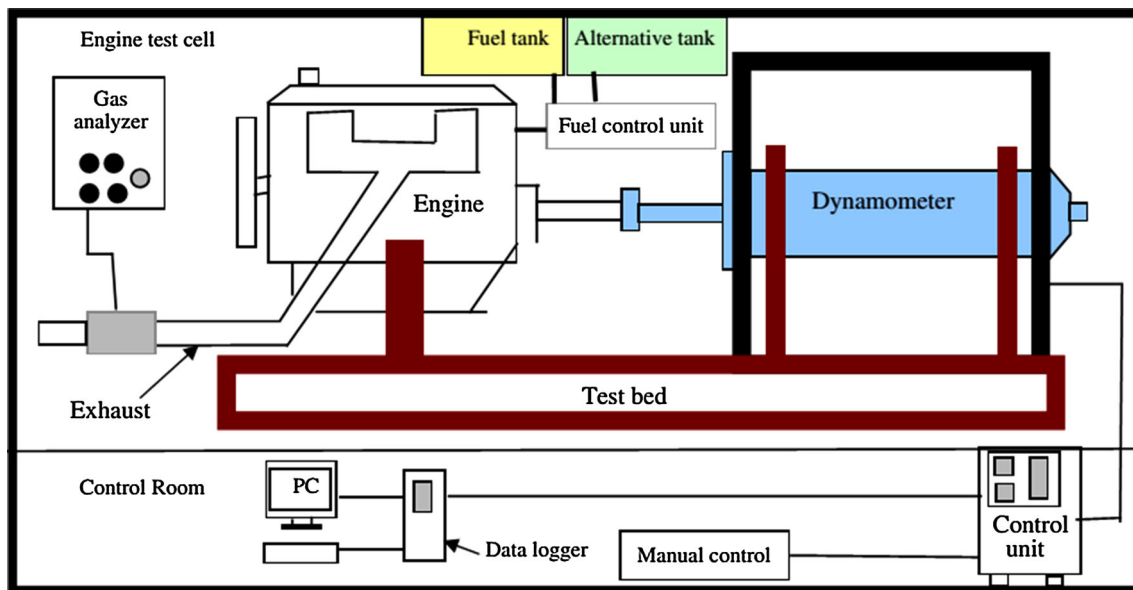
Tests were implemented in seven modes by the dynamometer (Table 2), and to ensure the results and its repeatability, the tests were repeated twice. Figure 1 is a schematic picture of experimental set-up. The degree of the machine's precision in measurement has been expressed in Table 3.

**Table 1** Properties of engine MF399

Model	A63544
Company	Motorsazan-Iran
Number of cylinders	6
Bore	98.6 mm
Stroke	127 mm
Cubic capacity	5.8 l
Max power at 2,300 RPM	82 kW (110 HP)
Max torque 1,300 RPM	376 Nm
Combustion sequence	1,5,3,6,2,4
Combustion system	Direct injection
Cooling system	Air cooled
Compression ratio	16:1
Injection time	22 BTDC

## Results and discussion

As seen in Fig. 2, the fuel consumption has the highest reduction when 10 and 20 ppm of nanoparticles were added to the fuel. Results of comparing different combinations between modes showed that the maximum fuel consumption for all fuels occurs at the sixth mode and the lowest fuel consumption occurs at the seventh mode. The maximum fuel consumption of 385 (ml/min) corresponds to diesel and nanosilver blend with a ratio of 40 ppm in mode 6, and minimum fuel consumption of 116 (ml/min) is related to diesel and nanosilver blend with a ratio of 10 ppm in mode 7. In terms of decreasing trend of the fuel consumption rate for diesel fuel, a decrease of approximately 1–2 % was achieved in most of the compounds. According to Fig. 2, the fuel consumption was decreased by increasing the amount of nanoparticles up to 20 ppm. Better fuel distribution in the combustion chamber, shortening of the ignition delay, and promoting the fuel's physical characteristics are among factors which lead to the reduction in the fuel consumption as a result of nanoparticles addition. As deduced by Fig. 2, the fuel consumption trend shows a slight reduction from base diesel to DAG10 that can be explained by the reduction in cohesion force between diesel fuel molecules by introducing nanoparticles resulting in lower fuel injection from the injector via viscosity decrement for the fuel. In contradiction, increasing the nanoparticle concentration (10–40 ppm) yields formation of denser droplets and ligaments through stronger adhesion bonds between fuel molecules and nanoparticles that is conducive to issuing more fuel from injector's nozzle tip. Nanoparticles inclusion in diesel fuel can enhance the momentum of fuel jet injection and the fuel penetration rate in the cylinder, which ultimately produces more uniform air/fuel mixture distribution in the combustion chamber. This outcome is in agreement with similar



**Fig. 1** Schematic picture of experimental set-up

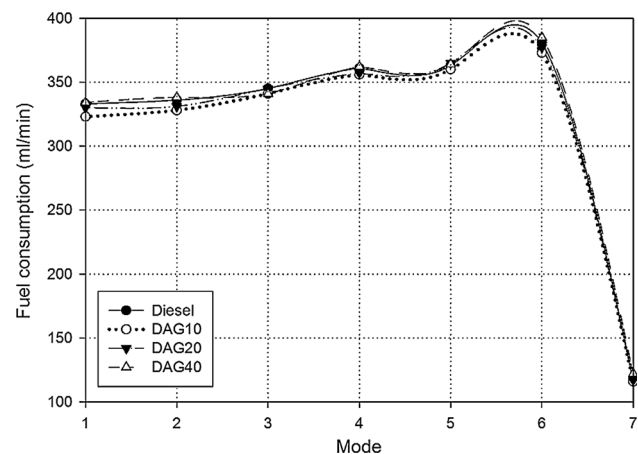
**Table 2** Engine test modes

Mode	Engine speed (RPM)
1	1,330
2	1,425
3	1,520
4	1,615
5	1,710
6	1,805
7 (idle)	1,900

investigations reporting better charge characteristics while nanoparticles were involved (Yang et al. 2013; Kao et al. 2008; Selvan et al. 2009).

The reason of the increased fuel consumption at 40 ppm mode can be attributed to the increase in viscosity and thereafter an increase in the droplets diameter during the fuel spraying. The maximum reduction rate of 3 % was associated to D10 fuel, and the maximum increase rates of 4.3 and 1 % were associated with D40 fuel in mode 7 and D40 fuel in mode 6, respectively. Indicated values by dynamometer in modes 3 and 5 suggest the highest values in terms of the engine torque and power. Regarding the specific fuel consumption, the mentioned cases prevail from economical standpoint when tests run in these modes.

As seen in Fig. 3, the CO emission in relation to the base fuel mode has a perceptible reduction with respect to enhanced mixture by nanoparticles. This outcome is in accordance with similar investigations taking nanoparticles in fuel composition (Basha and Anand 2010; Selvan et al. 2009; Solero 2012). The nanoparticle free fuel has



**Fig. 2** Variation of FC with respect to speed modes

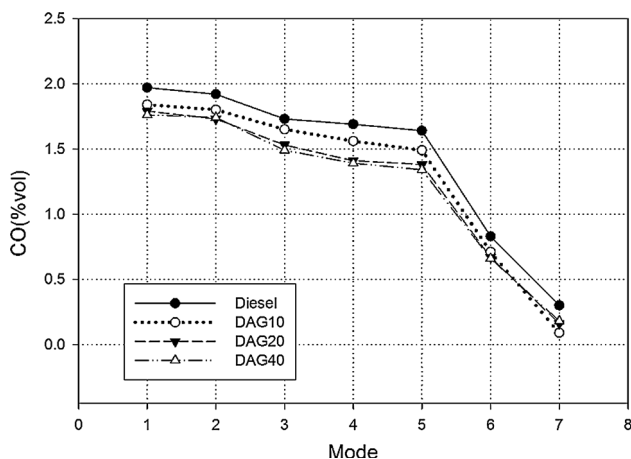
substantially higher CO emission, which is attributed to the cohesion inter-molecular bonds of diesel. Increasing the nanoparticle percentage involvement decreases the homogeneity of base fuel composition, thus expediting fuel disintegration and breakup during fuel injection. More fuel breakup causes better air–fuel mixture and reduction in equivalence ratio, which ultimately can decrease the CO emitted with DAG40 fueled engine.

In most cases, the approximate 20.48 and 40–70 % fuel consumption reduction was obtained compared to that of the base diesel fuel for D40, respectively, in loading conditions of dynamometer and idle mode (mode 7).

In the high loads of the dynamometer, the engine reaches to the smoke limit, hence the CO and UHC (unburned hydrocarbons) emissions increase in all of the

**Table 3** Measurement precision

Parameters	Accuracy
Engine speed	±1 rpm
Engine torque	±1 Nm
NOx emissions	±5 %
CO emissions	±1 %
CO <sub>2</sub> emissions	±2 %
HC emissions	±2 %
Fuel flow rate measurement	±1 %
Lower heating value of the fuel	±4 %

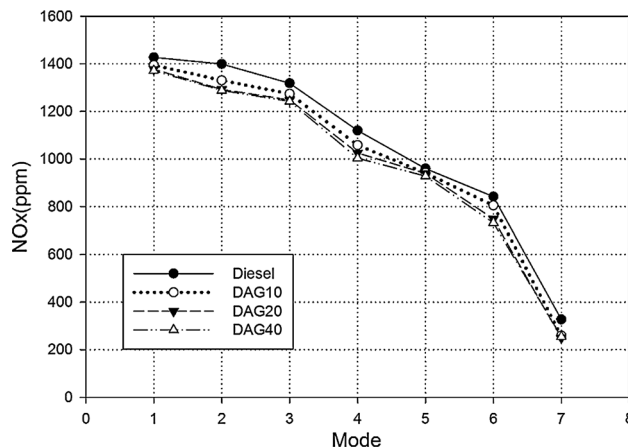


**Fig. 3** Variation of CO with respect to various modes

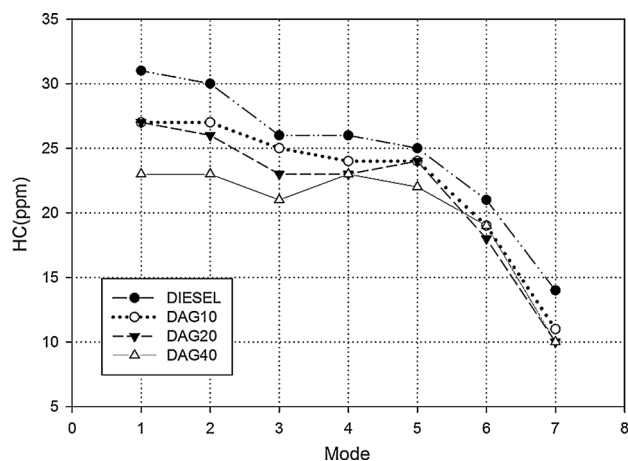
fuels. This is due to the oxygen shortage for the engine’s operation in the air/fuel ratio higher than unity (stoichiometric). The rate of changes after D20 is very low and adding more nanoparticles has no significant effect.

As seen in Fig. 4, silver nanoparticles have declining effect on NOx and it keeps decreasing up to 13 % for D40 in loading conditions of dynamometer and 20–23 % in idle mode (mode 7). Maximum NOx of 1,427 ppm is related to diesel fuel in mode 1, and minimum NOx of 250 ppm is related to the composition of the diesel and nanosilver with a ratio of 20 ppm in mode 7.

Numerous factors give rise to the particular formation of NOx emissions. According to the Zeldovich mechanism, the formation of NOx is dependent on oxygen concentration, residence time, and temperature (Benson and Whitehouse 1983). The temperature decline in the combustion chamber as a result of adding nanoparticles accounts for the NOx reduction. This outcome is in agreement with similar investigations that were carried out for nanoparticles (Yang et al. 2013; Kao et al. 2008; Basha and Anand 2010; Selvan et al. 2009; Sajith et al. 2010; Basha and Anand 2011). As known, the nanoparticles feature



**Fig. 4** Variation of NOx with respect to various modes



**Fig. 5** Variation of HC with respect to various modes

exceptional capability of heat transfer. One of the pivotal advantages of nanoparticle addition is its potential in decreasing the combustion chamber temperature with high rate of convective heat transfer increasing nano fraction in fuel leads to lowering the NOx emission.

UHC is considered as an emission that actively affects the engine efficiency unfavorably. Unburned or incomplete burned hydrocarbons were generated as a result of insufficient air accessible during fuel combustion. HC emission has been affected the most by application of metallic nanoparticles. According to Fig. 5, HC emission has a range of 4–28 % reduction and with the increment of silver amount will be reduced for all fuels with respect to the base fuel. This result can be corroborated with the reported studies of Yang et al. 2013, Kao et al. 2008, Basha and Anand 2010, Selvan et al. 2009, Sajith et al. 2010, and Basha and Anand 2011. However, due to the low content of HC in the operated diesel engine, the reduction in HC is of minor importance. The higher percentage of incomplete

combustion in the combustion chamber leads to the generation of UHC especially at higher equivalence ratio and hence a considerable efficiency decrement. As mentioned, nanoparticle involvement enhances the air–fuel mixing process and lower equivalence ratio, which brings about complete combustion, therefore higher thermal efficiency. The more nanoadditive, the more fuel spray droplet interaction and fuel droplet propagation.

The addition of silver nanoparticles to the fuel can widen the spray cone angle and facilitate the injected fuel's dispersion in the combustion chamber. The metallic particle existence in the pure liquid fuel with different density and momentum in the injection period along with their interaction accounts for better spray dispersion. On the other hand, establishment of a more complete combustion due to the more oxygen availability and silver properties would decrease these pollutants that were illustrated in Figs. 5, 6, 7. As indicated in former discussions, applying nanoparticles incurs reduction in fuel cohesion resulting in easier fuel breakup and creating smaller droplets or lower Sauter mean diameter, hence exposing more fuel surface to  $O_2$  oxidizer and thereby higher  $CO_2$  production.

$CO_2$  emissions are depicted as a function of various dynamometer loads for different fuel blends of nanoparticle portions in Fig. 6. As seen,  $CO_2$  emission resulted from nanoparticle-containing fuels is higher than that of pure diesel fuel at different dynamometer loads.

For the more oxygen availability and catalytic activities, existence of a fraction of nanoparticles improves spray quality and combustion phase which will increase  $CO_2$  emission concentration and thus decreases the emissions amount of CO and UHC incomplete combustion products.

Metals were often used as reducing catalysts rather than a catalyst for oxidation. But silver is an exception and was also used as an oxidation catalyst (Claus and Hofmeister 1999; Kvittek and Robert 2005; Prucek et al. 2004). Therefore, the application of this metal is suitable for the oxidation of organic compounds and also reducing nitro compounds and many others as well. On the other hand, the high surface area and surface energy will increase the performance of metallic nanoparticles. Any material involving the catalytic activity certainly has a high contact surface area. Because the surface of nanomaterials increases with decreasing the size, these materials are extensively used in catalysis. For example, in a crystal with a diameter of 10 nm, 15 % of the atoms are located on the surface, whereas in the nanocrystals with 1 nm diameter, all of the atoms are placed on the surface area. So a small nanocrystal with high surface will have more catalytic activity (Claus and Hofmeister 1999).

It can be inferred from the charts (with the exception of HC) that variation of emissions for higher nanofraction than D20 is little and it remains almost monotonous.

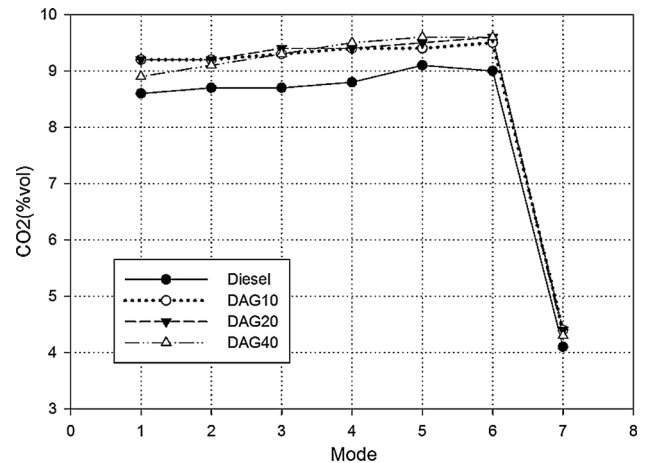


Fig. 6 Variation of  $CO_2$  with respect to various modes

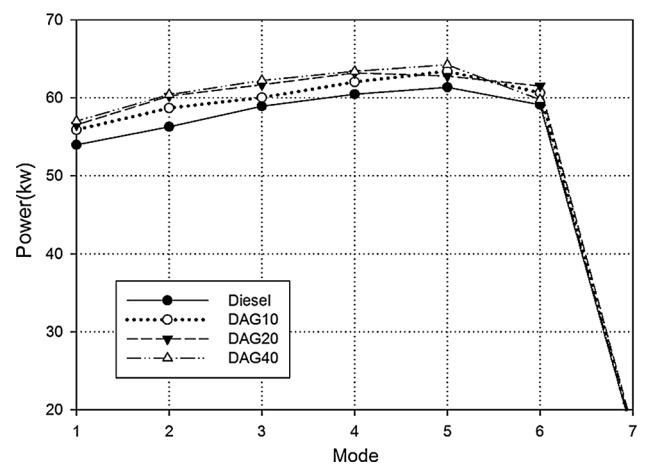


Fig. 7 Variation of Power with respect to various modes

Therefore, adding nanoparticles to diesel fuel was implemented up to 40 ppm.

According to Fig. 7, brake power increases with adding nanoparticles in fuel combination which implies fuel combustion improvement and higher rate for fuel energy conversion into useful work.

The engine power has increased in the range of 1.1–7.3 % tolerance compared to the base fuel. This outcome is in agreement with similar investigations using nanoparticles (Yang et al. 2013; Kao et al. 2008; Basha and Anand 2010; Selvan et al. 2009; Sajith et al. 2010; Basha and Anand 2011).

Results of comparing combinations between modes showed that the maximum power for all fuels occurred in the fifth mode and the lowest power occurred in the seventh mode. The maximum power of 64.2 kW is associated with diesel and nanosilver blend with a ratio of 40 ppm in mode 5 and minimum power of 16.7 kW is associated with net diesel in mode 7. In terms of power increase rate of diesel

fuel, a growth of approximately 4 % was achieved in most of the compounds. According to Fig. 7, the power has been increased by increasing the amount of nanoparticles, but this growth rate has been decreased after adding 20 ppm of nanoparticles and it was demonstrated that the addition of nanoparticles over this threshold has no significant impact on power. Maximum growth rates of 7.3 and 7 % for D40 and D20 fuels were achieved in mode 2, respectively. The minimum growth rates of 1.1 and 1.3 % were associated with D40 fuel in mode 6 and D10 fuel in mode 7, respectively.

Because of the above-mentioned reasons and the existence of metallic particles inside the chamber, better air/fuel mixture is expected, and additionally because of the catalytic role of the silver, the higher rate of energy release is certified. This increase could be due to the increased energy produced in the cylinder as increasing the surface to volume ratio of nanoparticles and increasing the heat transfer coefficient with nanoparticles in the fuel.

## Conclusion

Based on the obtained results from the experiments and diagrams, it was observed that adding silver nanoparticles to the diesel fuel will improve the fuel consumption and the extent of emitted pollution. Adding the metallic particles will increase the fuel infiltration and mixing with air, that this improves the combustion process. Also, these metallic particles will accelerate the fuel evaporation and will reduce the ignition delay in the combustion process.

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